

# 淮南玛纳斯地区低阶煤储层特征 及压裂改造效果研究

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**内容提要:**基于中国地质调查局组织施工的2口煤层气参数井资料,分析了准噶尔盆地南缘玛纳斯地区煤储层特征,综合影响煤层气富集与开发的储层参数,优选2#、5#煤层段采用大液量、中高排量、低砂比、变粒径支撑剂、多级阶梯式加砂压裂工艺进行储层改造,并采用地面微地震监测方法评价了压裂效果。研究表明:研究区中厚煤层群发育,煤层总厚度大、层间距小,且主要为原生结构的长焰煤。煤岩显微组分以镜质组和惰质组为主,储层微观孔隙发育,且主要为组织孔和溶蚀孔。煤储层孔隙度8.8%~14.5%,比表面积0.624~9.585 m<sup>2</sup>/g,孔容较大,孔隙连通性较好,渗透率0.0012~1.9286×10<sup>-3</sup> μm<sup>2</sup>,属中高孔—中低渗型储层。区内2#、5#煤层埋深大、含气量高、储层压力与能量高,但压裂施工中注入压力高,加砂效率低,储层改造难度较大。微地震监测结果显示,压裂所产生的人工裂缝以垂直缝为主,呈SE—NW展布,裂缝长度、宽度及影响体积都较大。压后放溢流时,放喷口气体可点燃,初步显示研究区具有良好的产气潜力。

**关键词:**玛纳斯;低煤阶;煤层气;储层特征;压裂改造

受美国粉河等盆地低煤阶煤层气商业开发成功的启示,低煤阶煤层气正成为国内研究的热点和勘探开发的新领域(崔思华等,2007;蔚远江等,2008;孙平等,2009)。新疆地区低煤阶煤层气资源丰富,2000 m以浅煤层气地质资源量约9.51×10<sup>12</sup> m<sup>3</sup>,占全国资源总量的26%。其中,准噶尔盆地南缘是煤层气最为富集的地区,也是煤层气“十三五”规划的重点战略突破区。近年来,自治区政府委托新疆煤田地质局等单位于盆地南缘东部阜康—白杨河矿区施工生产试验井51口,单井最高产气量达6200 m<sup>3</sup>/d,建成了年产能3×10<sup>7</sup> m<sup>3</sup>的煤层气开发利用先导性示范工程,对区域煤层气商业开发起到带动作用(张宇航,2017)。以玛纳斯矿区为富煤中心的盆地南缘中西段煤层气资源条件优越(伏海蛟等,2015;韩旭等,2017),但地质研究及资源评价程度极低,制约了区内煤层气勘探开发工作开展。本文依托中国地质调查局新疆公益性煤层气基础地质调查项目2口煤层气参数井资料,分析了盆地南缘玛纳斯地区低阶煤储层特征,探讨了煤储层可改造性及改造效果,以期为区内煤层气勘探开发工作提供理论与工程借鉴。

## 1 研究区地质背景

玛纳斯地区位于淮南煤田西段,东起呼图壁河,西至霍尔果斯河,北接昌吉凹陷,南以准噶尔地块南缘断裂为界,总体呈NW—SEE展布,东西长约89 km,南北宽10~19 km,面积约11500 km<sup>2</sup>。研究区构造位置位于准噶尔盆地南缘三排构造的第一排,霍玛吐背斜带与齐古断褶带中段,自西向东依次发育南玛纳斯向斜、清水河向斜(陈书平等,2007;白斌,2008),地层倾角13°~24°,构造相对简单,断裂不发育(图1)。研究区自下而上发育石炭系、二叠系、三叠系、侏罗系、白垩系、古近系、新近系及第四系。区内中侏罗世发育陆相湖泊—三角洲—沼泽沉积体系,湖盆水体较浅,气候温暖湿润,有利于陆生植物生长、沉积与保存,造就了中侏罗统西山窑组多煤层呈组呈群叠置发育,且煤层保存条件相对较好(田继军等,2011)。受古构造和沉积条件控制,煤层平面上呈北厚南薄、东厚西薄的趋势,具有近盆缘煤层多且厚度大、向盆内煤层数减少变薄的变化特征,聚煤中心在玛纳斯河与达西河一带。纵向上,具有煤层多、呈组呈群赋存、总厚度大、层间距小的特点(图2)。其中,2#、5#、6#、8#、9#、10#煤层厚度1.9

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~9.5 m,区内发育连续稳定,埋深在 800~1500 m,有利于煤层气富集与开采。

## 2 煤储层特征分析

### 2.1 煤岩煤质特征

区内施工的2口煤层气参数井—玛煤参1井、玛煤参2井西山窑组煤芯采样测试结果显示:目的煤层以原生结构煤为主,层内局部夹碎裂结构、碎粒结构及粉粒结构的构造煤。煤岩宏观组分以亮煤、半暗煤为主,暗煤、镜煤少量,属于半亮—半暗型煤。显微煤岩组分以镜质组为主,含量介于31.40%~76.50%,平均59.61%,较高的镜质组有利于煤层气的生成与储集;惰质组含量介于10.50%~59.30%,平均19.61%;壳质组含量低,一般为0.30%~0.56%。煤的镜质组最大反射率 $R_{o,max}$ 介于0.50%~0.85%,以低煤阶长焰煤为主,煤系下段含中等变质程度的气煤。煤的视密度1.25~1.57 g/cm<sup>3</sup>,真密度1.38~1.66 g/cm<sup>3</sup>;煤层水分1.04%~1.49%,平均为1.29%;灰分3.23%~18.39%,硫分0.30%~1.32%,挥发分35.45%~47.95%。

### 2.2 煤层含气性

区内2口煤层气参数井采集的36个煤芯样含气性测试结果显示:各煤层空气干燥基含气量0.89~6.43 m<sup>3</sup>/t,平均3.66 m<sup>3</sup>/t。尽管煤阶较低的影响,煤层含气量整体不高,但仍普遍高于褐煤—长焰煤空气干燥基含气量1 m<sup>3</sup>/t工业下限标准,且含气

量随埋深增加呈逐渐升高的趋势,较高的含气量是煤层气富集重要条件。煤层气组分以CH<sub>4</sub>为主,占77.10%~94.79%,平均为84.04%;其次为N<sub>2</sub>,占4.18%~25.37%,平均14.58%;CO<sub>2</sub>、乙烷极少;气体组分随煤层埋深增加变化不明显。平衡水煤样干燥无灰基兰氏体积5.32~28.76 m<sup>3</sup>/t,平均14.28m<sup>3</sup>/t,兰氏压力1.52~4.89 MPa,平均3.57 MPa(图3);兰氏压力较高,易于煤层气的解吸及产出。综合含气量、等温吸附及试井所获得的储层压力数据,计算煤储层临界解吸压力为1.64~4.19 MPa,理论含气饱和度61.2%~81.7%,平均71.2%,临储比0.39~0.76,反映区内煤层具有含气饱和度高、临界解吸压力高、临储比高的特点,具备煤层气地面开发的条件。

综合以往煤田勘探钻孔及2口煤层气参数井的资料,发现同一钻孔中各目的煤层含气量差异较大,且垂向变化无明显的规律性;平面上,各煤层含气量随埋藏深度增加呈增大的趋势。上述含气量空间变化,垂向上反映出典型的多层叠置统一含煤层气系统特征(秦勇等,2008)。平面上,研究区受构造和沉积双重控制及断层影响,含气量表现出南低北高、西低东高的变化规律。

### 2.3 孔裂缝发育特征

基于煤岩芯录井及扫描电镜、压汞、低温液氮吸附等实验测试,研究了主要目的煤层孔裂隙特征发育特征。结果表明:煤储层外生裂隙多呈不规则网

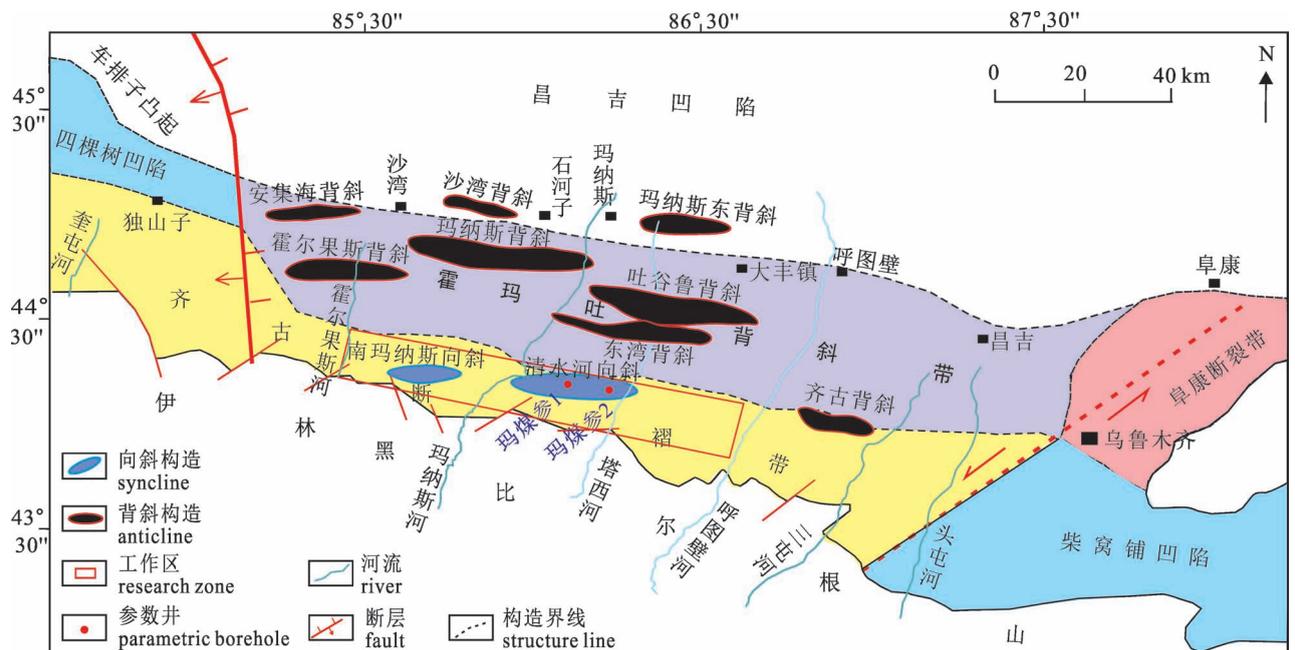


图1 玛纳斯地区构造纲要图

Fig. 1 Structure outline map of Manas area

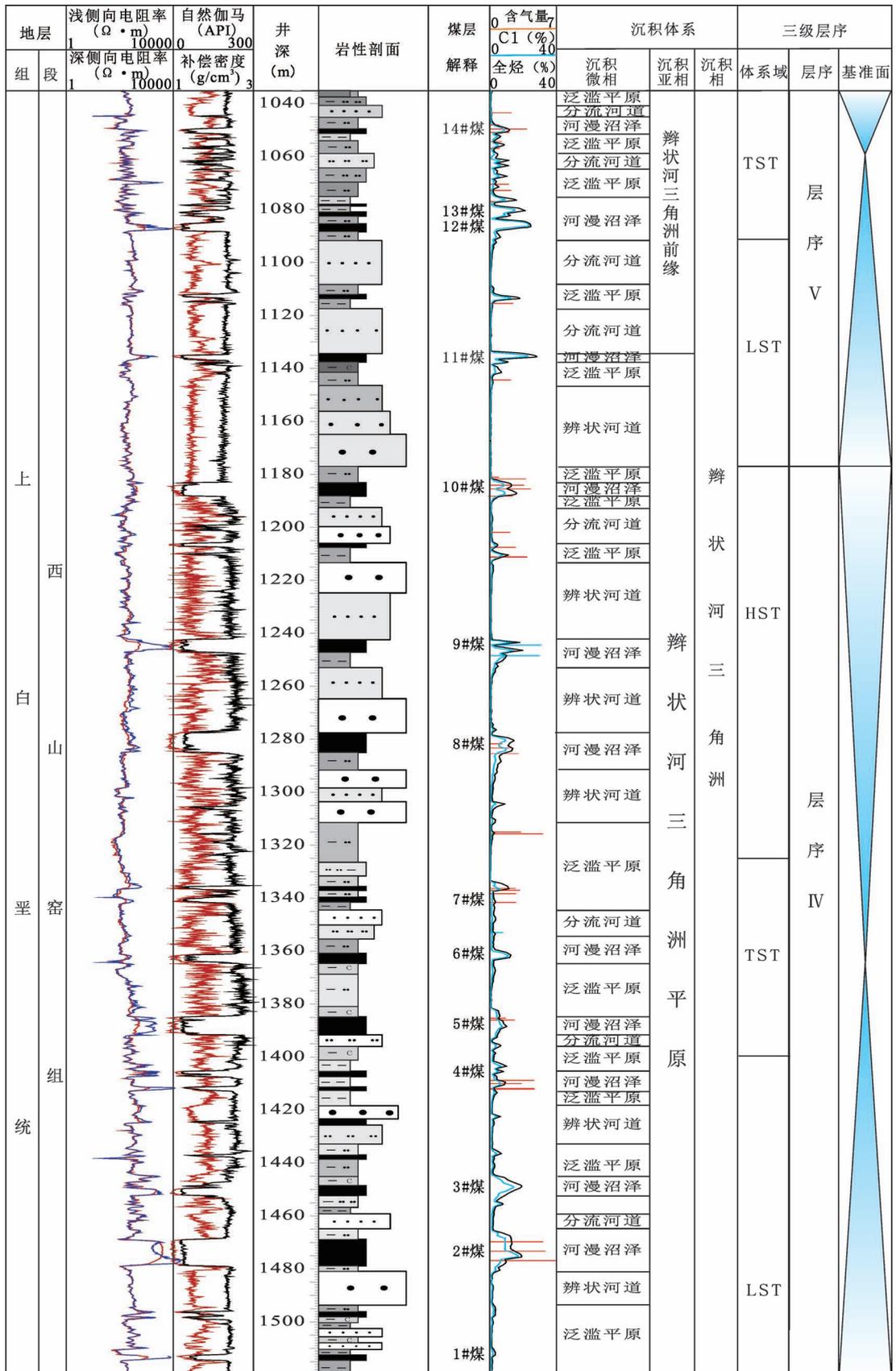


图 2 玛纳斯地区含煤地层综合柱状图  
Fig. 2 Coal bearing strata column of Manasi area

状、碎裂状,矿物充填少,连通性中等(图4a、b);裂隙平均密度26~69条/mm,长度0.1~8.8 mm,高度0.1~9.2 mm,宽度2~39 μm。内生裂隙主要发育在镜质体中,定向性明显,多平行于层理展布(图4c);内生主裂隙平均密度为8~18条/mm,长度0.2~4.1 mm,高度0.1~12.0 mm,裂隙宽度1~39 μm。煤的孔裂隙类型多样,且以原生结构孔和矿物质溶蚀孔为主,同时还发育少量屑间孔、摩擦孔、角砾孔等(图4d、i),形状不规则,少量被方解石充填,孔径集中在6~90 nm;煤层BET比表面积为0.624~9.585 m<sup>2</sup>/g,平均为3.407 m<sup>2</sup>/g,BJH总孔体积平均为0.00601 mL/g,平均孔径为5.83 nm。

总体来看,研究区主要目的煤层气体储集空间类型多样,孔隙以微孔、小孔为主,孔裂隙充填少,裂缝开启性好,总体上有利于煤层气的吸附与渗流(傅雪海等,2001)。

### 2.4 煤储层渗透性

根据玛煤参2井注入压降试井结果,2#、5#、10#煤层试井渗透率分别为0.0035×10<sup>-3</sup> μm<sup>2</sup>、0.2686×10<sup>-3</sup> μm<sup>2</sup>、1.9286×10<sup>-3</sup> μm<sup>2</sup>,各煤层渗透率存在较大差异。同时,实验室覆压孔渗法测定2#、5#、10#煤层孔隙度分别为8.8%、11.6%、14.5%,渗透率分别为0.0012×10<sup>-3</sup> μm<sup>2</sup>、0.046×10<sup>-3</sup> μm<sup>2</sup>、0.457×10<sup>-3</sup> μm<sup>2</sup>。尽管各煤层渗透率的相关高低关系一致,但实验室测得的渗透率明显低于试井法获得的渗透率,这可能与钻井过程中煤层段扰动裂隙产生有关。综合,试井法与覆压孔渗法的测试结果,研究区主要目的煤层属于中高孔—中低渗型煤储层,储层微孔发育、孔径较小是导致渗透率偏低的主要原因(叶建平等,1999)。此外,受煤系下部煤储层压力增大的影响,研究区煤储层孔隙度、渗透性随埋深

增大而降低的规律性明显。

### 2.5 温压条件与岩石力学特征

玛煤参1井、玛煤参2井注入/压降试井显示:西山窑组主力煤层煤储层温度32.36~42.11℃,储层压力介于12.21~15.18 MPa,储层压力梯度1.01~1.03 MPa/100 m,煤层破裂压力19.60~23.76 MPa,破裂压力梯度1.49~1.71 MPa/100 m,闭合压力18.74~19.55 MPa,闭合压力梯度1.41~1.58 MPa/100 m。垂向上,储层温度、储层压力随深度增加而逐渐增大,而压力梯度基本不变,表明该区为多煤层叠置正常单一的地层压力系统,避免了合层排采过程中层间干扰,有利于多煤层合采条件下最大限度开发煤层气资源(杨兆彪等,2013)。

煤层及顶底板岩石力学特征测试显示:主力煤层抗压强度5.7~13.0 MPa,平均8.91 MPa;抗拉强度0.39~5.36 MPa,平均2.99 MPa;弹性模量1.86×10<sup>3</sup>~2.92×10<sup>3</sup> MPa;平均2.09×10<sup>3</sup> MPa;泊松比0.31~0.54。顶底板岩石抗压强度25.3~57.2 MPa,平均36.5 MPa;抗拉强度3.45~8.98 MPa,平均4.61 MPa;弹性模量6.72×10<sup>3</sup>~30.3×10<sup>3</sup> MPa,平均26.1×10<sup>3</sup> MPa;泊松比0.19~0.22。顶底板抗压强度、抗拉强度比煤层大,弹性模量比煤层小,抗压性和抗拉性均优于煤层;煤层泊松比明显高于顶底板泥岩、粉砂质泥岩和碳质泥岩,有利于水力压裂时煤层中裂缝的产生、扩展与控制。合理控制压裂施工参数,将有效防止裂缝沟通顶底板含水层,提高煤储层渗透性改造效果。

## 3 储层压裂工艺与效果评价

区内中侏罗统西山窑组发育煤层多、层间跨度大、含气量不高,单层开发不具经济性,分段压裂、合

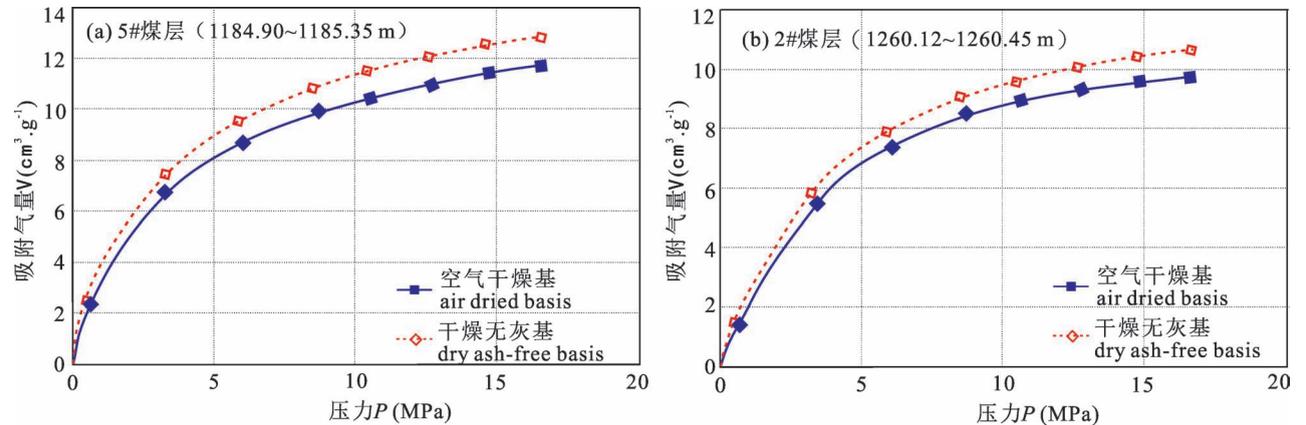


图3 玛煤参1井主要煤层等温吸附实验曲线图

Fig. 3 Isothermal adsorption curve of main coal seams in Mameican-1 well

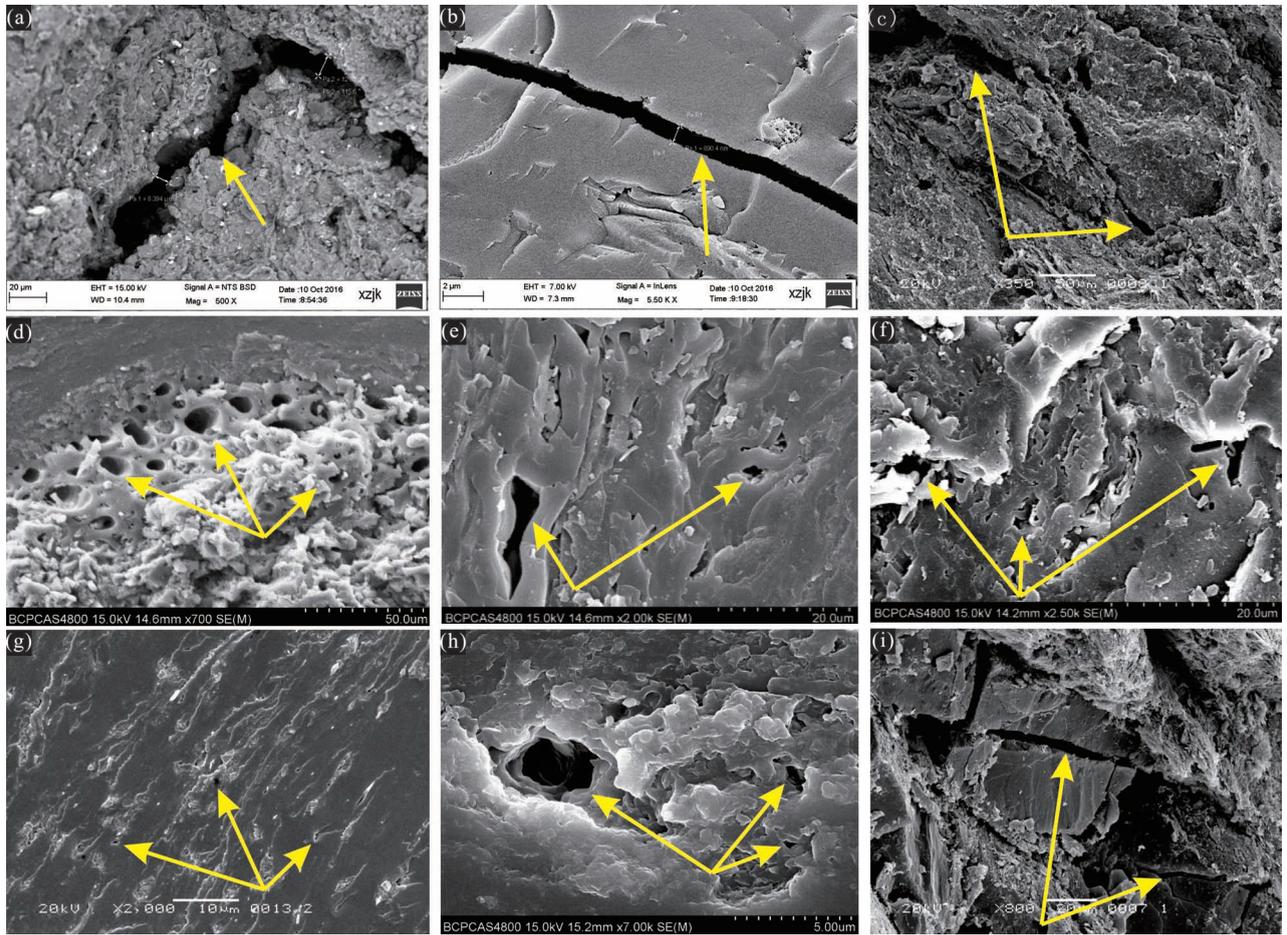


图4 玛纳斯地区煤样微观孔裂隙扫描电镜照片

Fig. 4 SEM images of microscopic pore and fracture in coal samples selected from Manas mining area

(a) 外生裂隙; (b) 外生裂隙; (c) 内生裂隙; (d) 结构孔; (e) 结构孔; (f) 结构孔和屑间孔;  
(g) 摩擦孔; (h) 溶蚀孔; (i) 角砾孔

(a) exogenic fracture; (b) exogenic fracture; (c) endogenic fracture; (d) constructional pores; (e) constructional pores;  
(f) constructional pores and interclast pores; (g) friction pores; (h) dissolved pores; (i) brecciated pores

层排采是大幅提高煤层气井产气量的有效途径(汪万红等,2014;罗开艳等,2016)。由于研究区煤层气藏为多煤层叠置单一压力系统型,因此在一定程度上避免了多煤层合采时的层间干扰问题。以影响多煤层合采可行性的煤层含气量、临界解析压力、渗透率、储层压力等储层关键参数的优越性、相近性为基本原则(彭龙仕等,2014;敖显书等,2016),优选煤体结构完整、含气量高、渗透性好、临储比高且相近的2#和5#煤层进行分层射孔压裂及合层排采,探索与区域煤层气地质条件匹配的煤层气开发技术。

### 3.1 压裂改造工艺及储层响应

基于煤系煤层群发育特点及研究区储层发育特征,综合煤储层敏感性测试及压裂液配伍试验结果,设计采用光套管注入水力压裂方式,大液量、中高排

量、低砂比、变粒径支撑剂、多级阶梯式加砂压裂工艺进行煤储层活性水水力压裂改造。结合压裂曲线分析与地面微地震裂缝监测,评价研究区煤储层可改造性及改造效果。

2#煤层射孔段为1469.8~1476.8 m,压裂施工排量8.3~9.5 m<sup>3</sup>/min,平均排量9.0 m<sup>3</sup>/min;施工泵压30.8~37.5 MPa,累积注入压裂液2226 m<sup>3</sup>。其中,前置液量461 m<sup>3</sup>,前置液阶段泵注砂比为3%、5%、7%的细砂段塞;携砂液量1765 m<sup>3</sup>,携砂液阶段砂比3%~9%,总砂量61 m<sup>3</sup>。根据压裂曲线,2#煤层破裂压力34.5 MPa,闭合压力为19.6 MPa(表1)。5#煤层射孔段为1385.8~1392.8 m,压裂施工排量8.6~9.5 m<sup>3</sup>/min,平均排量9.1 m<sup>3</sup>/min;施工泵压19~26 MPa,累积注入压裂液1202 m<sup>3</sup>。

其中,前置液量  $511 \text{ m}^3$ ,前置液阶段泵注砂比为4%、6%、8%细砂段塞;携砂液量  $691 \text{ m}^3$ ,携砂液采用砂比6%~16%中砂,阶梯式注入,平均砂比10.5%,总砂量  $75 \text{ m}^3$ 。根据压裂曲线,5#煤破裂压力  $25.1 \text{ MPa}$ ,闭合压力为  $6.2 \text{ MPa}$ (图5)。

表1 玛煤参2井水力压裂施工参数

Table1 Parameters of hydraulic fracturing operation in Mameican-2 well

压裂煤层		2#煤	5#煤
射孔井段(m)		1469.8~1476.8	1385.8~1392.8
施工排量( $\text{m}^3/\text{min}$ )		8.3~9.5/9.0	8.6~9.5/9.1
加砂量( $\text{m}^3$ )		61	75
砂比(%)		4~8/5	6~16/10.5
压裂液量	总液量( $\text{m}^3$ )	2226	1202
	前置液量( $\text{m}^3$ )	461	511
	携砂液量( $\text{m}^3$ )	1765	691
前置液占比(%)		20.7	42.5
破裂压力(MPa)		34.5	25.1
闭合压力(MPa)		19.6	6.2

2#煤层埋深较大、煤储层压力和破裂压力高且局部夹粉煤,压裂施工中进液难、滤失大、加砂效率低,表现为2#煤层泵注携砂液阶段产生两次砂堵,通过停泵放喷才顺利解堵。针对煤储层上述压裂响应,5#煤改造时增加了前置液量及降滤失剂量,人造裂缝延展通顺、平稳;注携砂液阶段,采用多级阶梯式加砂,显著提高了活性水携砂能力及裂缝支撑效果,储层改造施工顺利,达到了压裂施工预期目标。

### 3.2 压裂效果分析

地面微地震裂缝监测显示,2#、5#煤层压裂所产

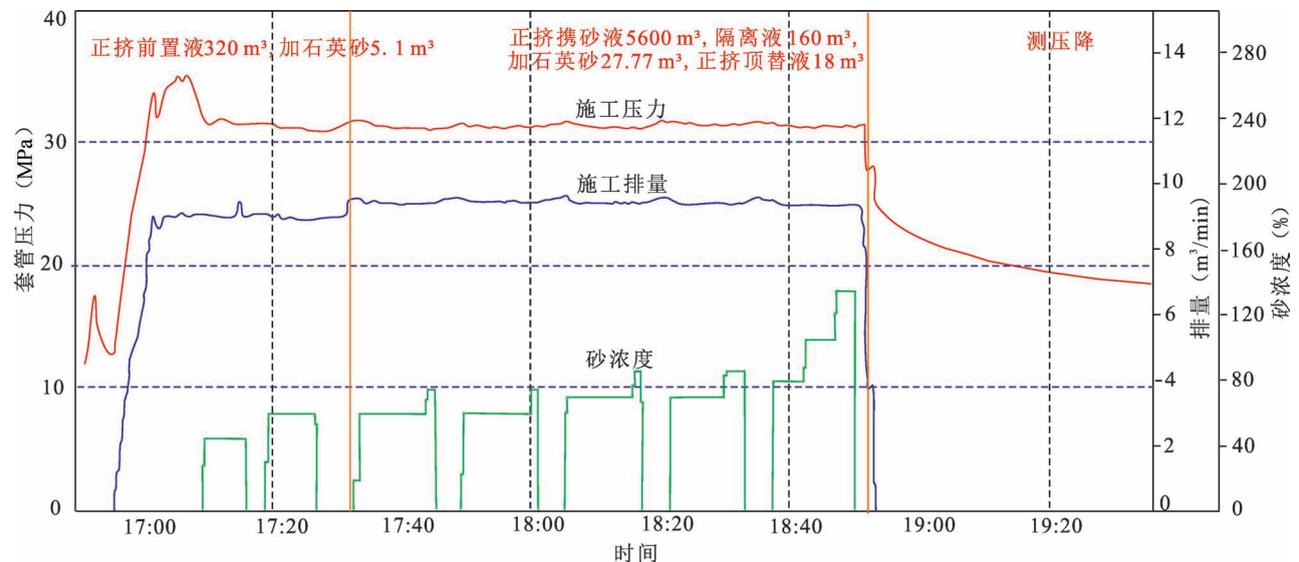


图5 玛煤参2井5#煤层压裂施工曲线

Fig. 5 Fracturing construction curve of 5# coalbed in Mameican-2 well

生的人工裂缝两翼均衡拓展,主方位为SE—NW向,与区域水平最大主应力方向一致。裂缝产状主要为垂直缝,单翼缝长  $90.5 \sim 142.2 \text{ m}$ ,裂缝宽度  $39.8 \sim 48.0 \text{ m}$ ,裂缝高度分别为  $19.1 \text{ m}$  和  $25.8 \text{ m}$ ,压裂改造体积约为  $22.74 \times 10^4 \sim 27.37 \times 10^4 \text{ m}^3$ ,将会有效的改善煤储层的联通性,提高煤层渗透率(康永尚等,2016),压后放溢流时,放喷口气体可点燃,火苗  $30 \sim 50 \text{ cm}$ ,表明水力压裂施工达到了预期的煤储层改造效果,揭示了玛纳斯地区低煤阶煤储层具有良好的产气潜力。

该井压裂完后,用5 mm油嘴放喷排采作业,初期日产水量为  $38 \sim 43 \text{ m}^3$ ,目前日产液量为  $19 \sim 20 \text{ m}^3$ ,累计出液  $8478.35 \text{ m}^3$ ,井口压力  $0.20 \text{ MPa}$ ,由于目标煤储层含水量大,液面未下降。为实现有效排采,玛煤参2井将下入日排水  $300 \sim 400 \text{ m}^3$  能力的电潜泵加强储层排水,达到的降压解吸产气的效果。

## 4 结论

(1)玛纳斯地区中侏罗统西山窑组中厚煤层群发育,煤层总厚度大、层间距小,且主要为原生结构的长焰煤。煤岩显微组分以镜质组和惰质组为主,储层微观孔隙发育,且主要为组织孔和溶蚀孔。煤储层孔隙度  $8.8\% \sim 14.5\%$ ,比表面积  $0.624 \sim 9.585 \text{ m}^2/\text{g}$ ,孔容较大,孔隙连通性较好,渗透率  $0.0012 \sim 1.9286 \times 10^{-3} \mu\text{m}^2$ ,属中高孔—中低渗型储层。

(2)玛纳斯地区2#、5#煤层埋深大、含气量高、储层压力与能量高,压裂施工中注入压力高、加砂效率低,储层改造难度较大。通过增加前置液量及降

滤失剂量,采用多级阶梯式加砂方式,可显著提高活性水压裂液造缝及携砂效果。

(3)玛纳斯地区煤储层水力压裂裂缝以垂直缝为主,呈SE—NW向展布,裂缝长度、宽度及影响体积都较大。压后放溢流时,放喷口气体可点燃,显示该区具有良好的产气潜力。

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## Low-rank CBM Reservoir Characteristics and Effects of Fracturing Reconstruction in the Manas Area, Southern Junggar Basin

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**Objectives:** The resource condition of low rank coalbed methane resources in Manas mining is superior. However, the degree of geological research and resource evaluation is extremely low, which restricted the exploration and development of coalbed methane in the area. The purpose of this study is to analyze the characteristics of the low-order coal reservoirs, and to discuss the reformability and effect of coal reservoirs Hydraulic fracturing, in order to provide theoretical and engineering reference for the exploration and development of coal bed methane in the area.

**Methods:** By two coalbed methane (CBM) parameter wells drilling and Core sample testing, Comprehensive analyzed the reservoir parameters which influence the enrichment and development of CBM, 2# and 5# coal seams were optimized for reservoir reconstruction Meanwhile, the micro-seismic monitoring method was used to evaluate the fracturing effect.

**Results:** The thickness and depth of coal seam in the Manas area is 1.9~9.5 m and 800~1500 m,  $R_{o,max}$  between 0.50% and 0.85%. gas content of air dried basis is 0.89~6.43 m<sup>3</sup>/t. The coal reservoir porosity is in the range of 8.8%~14.5% with the specific surface area is 0.624~9.585 m<sup>2</sup>/g. The pore has a large volume and good pore connectivity, with the permeability between 0.0012×10<sup>-3</sup> μm<sup>2</sup> to 1.9286×10<sup>-3</sup> μm<sup>2</sup>. Coal reservoir pressure ranges from 12.21 MPa to 15.18 MPa, break pressure ranges from 19.60 MPa to 23.76 MPa, which are beneficial to the enrichment and fracturing of coalbed methane. The reservoir reconstruction of 2# and 5# coal seam transformed fracture with a single wing length of 90.5~142.2 m, width of 39.8~48.0 m, volume of 22.74×10<sup>4</sup>~27.37×10<sup>4</sup> m<sup>3</sup>, and effectively improved coal reservoir connectivity and permeability.

**Conclusions:** The Medium—thick coal seam groups are developed in Manas area, with a large total thickness, a raw structure and mainly a kind of long flame coal. The microscopic pores of the reservoir are developed, which are mainly tissue pores and dissolution pores. The pore has a large volume, good pore connectivity, and medium—low permeability. The 2# and 5# coal seams in the study area have a large buried depth, a high gas content, a high reservoir pressure and formation energy. However, during the fracturing, the injection pressure is high and the sand adding efficiency is low which reflect the difficulty of reservoir reconstruction. The micro-seismic monitoring results show that the artificial fractures produced by fracturing are mainly vertical fractures, showing SE—NW striking, and the length, width and volume of the fractures are all relatively large. When the flood discharge is released after fracturing, the discharge gas can be ignited, which shows a good gas production potential in the study area.

**Keywords:** southern Junggar basin, manas, low-rank coalbed methane, reservoir characteristics, fracturing reconstruction

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