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## Calculation and thermodynamic analysis of log f(O<sub>2</sub>)-log a(SiO<sub>2</sub>) diagrams of the CaO-FeO-SiO<sub>2</sub>-O<sub>2</sub> system

SHI Xunli<sup>1</sup> and HU Jiawen<sup>2\*</sup>

1 School of Mathematics and Science, Shijiazhuang University of Economics, Shijiazhuang 050031, Hebei, P. R. China 2 College of Resources, Shijiazhuang University of Economics, Shijiazhuang 050031, Hebei, P. R. China

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The phenomena of magnetite (Mt, Fe<sub>3</sub>O<sub>4</sub>), andradite (Andr.  $Ca_3Al_2Si_3O_{12}$ ), hedenbergite (Hd,  $CaFeSi_2O_6$ ) exsolved from or intergrown with Ca-Fe-rich olivines that may be fayalite (Fa, Fe<sub>2</sub>SiO<sub>4</sub>), or kirschsteinite (Kst, CaFeSiO<sub>4</sub>), or their solid solutions have been found in many different geological settings, especially in Mg-poor cases. The relevant mineral assemblages often contain very pure wollastonite (Wo, CaSiO<sub>3</sub>), or Ca-rich pyroxene (such as augite), and sometimes intergrow with hematite (H, Fe<sub>2</sub>O<sub>3</sub>). In order to understand the geochemical behaviors of these minerals and their physicochemical conditions, it is necessary to get accurate phase diagrams of the relevant systems under different conditions. At present, there are many theoretical and experimental reports on the phase equilibria of these systems (Hu et al., 2011; Selleby, 1997; Sommacal, 2004), but they are all defective somewhat. For instance, owing to the lack of thermodynamic data of minerals, some studies were only qualitative or semi-quantitative (e.g. Kst) (Hu et al., 2011), even one or some phases or components mentioned above were not involved. What is more, some data of different precisions or reliabilities were simply used together in calculation. Considering the data from different sources may be inconsistent with each other, some results may be problematic. Recently, Sommacal (2004) optimized the data of Kst with the model of Holland and Powell (1998). This dataset of Kst and that of other minerals or components by Holland and Powell (1998), as well as the Fa-Kst solid solution model of Mukhopadhyay and Lindsley (1983), are adopted to calculate  $logf(O_2)-loga$ (SiO<sub>2</sub>) diagrams under different temperatures and pressures.

For a  $log f(O_2) - log a(SiO_2)$  phase diagram of the CaO-

FeO-SiO<sub>2</sub>-O<sub>2</sub> system under given temperature and pressure,  $f(O_2)$  and  $a(SiO_2)$  are essentially external condition variables that define the stability fields of mineral assemblages, so O2 and SiO2 can be removed by projecting the phase composition space (i.e. chemography) of the quaternary system from SiO<sub>2</sub> and O<sub>2</sub> to the subspaces without SiO<sub>2</sub> and O<sub>2</sub>, respectively (Hu, 2012; Hu et al., 2011), or can be eliminated together by matrix projection (Greenwood, 1975). As a result, the quaternary system is actually equivalent to a binary system in phase diagram topology (Hu, 2012). At given temperature and pressure, the CaO-FeO-SiO<sub>2</sub>-O<sub>2</sub> system has four phases in an invariant assemblage, and three phases in a univariant assemblage. In this work, all phase assemblages are labeled with their absent phases (Zen, 1966). For simplicity, the invariant points and univariant lines corresponding to the above assemblages are also labeled with the same symbols, respectively. According to the topological analysis theory of phase diagrams, if m extra phases are added to an invariant assemblage, it will result in form an *m*-grade (or *m*-level) multisystem (Hu et al., 2004; Hu, 1998).

The main steps of the phase diagram calculation can be summarized as follows:

Firstly, calculate the univariant lines. Balance each unvariant reaction defined by its univariant assemblage, and express it in standard form which means the form as " $0 = \sum v_B$ ", where  $v_B$  is the stoichiometric number of phase or component B in a reaction (which is negative for reactant, and positive for product). The molar Gibbs free energy (relative value) of every mineral or component can be calculated with the model of Holland and Powell (1998). The calculation of every univariant line is based on its corresponding chemical equilibrium condition. The calculated values of  $\log a(SiO_2)$  and  $\log f(O_2)$  are used to plot the  $\log a(SiO_2)-\log f(O_2)$  diagrams.

Secondly, discriminate the stable fields of reactant or product assemblages. For the  $logf(O_2)-loga(SiO_2)$ 

<sup>\*</sup> Corresponding author. E-mail: hu\_jiawen@sina.com.



Fig. 1. log/(O<sub>2</sub>)-log*a*(SiO<sub>2</sub>) diagrams of CaO-FeO-SiO<sub>2</sub>-O<sub>2</sub> system under constant temperatures and pressures.

diagrams in this work, almost all univariant reactions involve  $O_2$  or SiO<sub>2</sub>, or both of them. According to La Chaterlier's principle, the mineral assemblages on the side of  $O_2$  or SiO<sub>2</sub> can only be stable on the lower  $f(O_2)$  or a (SiO<sub>2</sub>) side.

Thirdly, determine the stable parts of the univariant lines. According to Schreinemakers' rules (Zen, 1966) and the results in the second step, if the reactant or product assemblage of an arbitrary reference univariant line contains phase B and is stable on one side of the univariant line, then the phase B-absent univariant line belonging to the same invariant assemblage can only be stable on the opposite side of the reference univariant line.

Finally, determine the stabilities of invariant points. According to the closed net theory of multisystems (Hu et al., 2004; Yin et al., 2002; Zen, 1966), the invariant points of a one-grade multisystem cannot be all stable under any given conditions. According to the stability theory of invariant points (Cheng and Greenwood, 1990; Hu et al., 2000; Lépine et al., 1992; Vielzeuf and Boivin, 1984), if an invariant point is passed through by the metastable part of a univariant line emanating from the invariant point, the invariant point and the univariant lines emanating from it must be all metastable.

The seven-phase system (a three-grade multisystem) in this work includes one-grade multisystems. Therefore, it would be very time consuming if we do all the above thermodynamic calculations and discriminations for each one-grade multisystem. We found a high-efficiency approach: (1) Choose an arbitrary one-grade multisystem as the initial system, do all the foregoing calculations and discriminations associated with reactant and product assemblages, univariant lines and invariant points; (2) Add a new phase to the system, and repeat the above calculation and discrimination for all one-grade multisystems that do not include the metastable invariant assemblage(s) determined in the preceding step. Finally, put all the stable parts of univariant lines together to form a complete phase diagram. In this way, a complete stable equilibrium phase diagram can be obtained with a small amount of calculation (Figure 1).

Through systematic analysis of the calculated phase diagrams, the following conclusions can be drawn: (1) Under given temperature and pressure, if  $f(O_2)$  is high

enough, Fa and Kst will change into minerals that are more oxidizing and/or richer in silica; at higher a(SiO<sub>2</sub>), the silica-rich minerals are more stable. (2) Temperature has much more notable influence on reaction equilibria than pressure. At constant pressure, as temperature drops, univariant lines and invariant points dramatically move towards to the direction of lower  $f(O_2)$  or  $a(SiO_2)$ . The drop of temperature can drive oxidation reactions, and the SiO<sub>2</sub> released from oxidation reactions can further drive some  $SiO_2$ -consuming reactions. Consequently, if temperature is low enough, Fa and Kst will spontaneously transform into oxidizing minerals or silica-rich minerals. These facts suggest that all reactions in the calculated phase diagrams have significant changes in entropy, because they involve  $O_2$  or  $SiO_2$ , or both of them. (3) It is found that the phase diagrams of one-grade multisystems {Fa, H} and {Wo, H} can change their configurations with temperature below the highest phase separation temperature (about 1040 °C) of Fa-Kst solid solution. The most attractive features of these changes are that the changes always happen in one-grade multisystems, and the relatively stable net and relatively metastable net of a onegrade multisystem always simultaneously change their stabilities as a whole. That is, if the relatively stable net becomes metastable, then the relatively metastable net will also become metastable. In The seven-phase system in this work undergoes two configurational transformations, which result in three configurations (Fig. 1). (4) Pressure has no remarkable influence on the positions of most reaction equilibrium lines, except for few ones. Nevertheless, the increase of pressure can raise the configurational transformation temperatures of phase diagrams, which has same effect as temperature decrease do, but not as notable as it.

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